

# PATENT SPECIFICATION

(11) 1 453 256

1 453 256

- (21) Application No. 19190/75 (22) Filed 7 May 1975  
(44) Complete Specification published 20 Oct. 1976  
(51) INT CL<sup>2</sup> C23C 17/00  
(52) Index at acceptance  
C7F 1A 1X 2F 2M 2P 2U 2Z2 3E 4A 4E 4F 4K 5A  
(72) Inventors YUKIO OTSUKI  
HIROYUKI MATSUMOTO  
HIROSHI ITO and  
SHUSUKE TAKEZAKI



## (54) A METHOD OF TREATING A SLIDING SURFACE USING WIRE-EXPLOSION COATING

- (71) We, KAWASAKI JUKOGYO KABUSHIKI KAISHA, a Japanese Body Corporate, of 14 Higashikawasaki-cho, 2-chome, Ikuta-ku, Kobe-shi, Hyogo-ken, Japan and NIPPON TUNGSTEN CO., LTD., a Japanese Body Corporate of 460 Aza Sannoh, Ohaza Shiobara, Minami-ku, Fukuoka-shi, Fukuoka-ken, Japan, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:—
- This invention relates to a method of treating a sliding surface using wire-explosion spray coating, and more particularly to a method using wire-explosion spray coating, according to which cylinders for use in internal combustion engines having good wear resistance, peel resistance and seizure resistance characteristics and uniform quality can be inexpensively mass-produced without co-production of an effluent which causes environmental contamination.
- Heretofore, cast iron cylinders or aluminium cylinders having a cast iron liner have been utilized as cylinders for use in internal combustion engines. However, in the modern high performance and high power engine, the conventional cylinder has become insufficient because of its poor cooling characteristics, and this has become a large problem in the production of engines. Recently, in order to overcome this problem, chromium plated aluminium cylinders having the inner sliding surface plated with chromium have been adopted for some applications. However, production of these cylinders relies on a plating process which produces a waste liquor effluent and thus entails the possibility of causing environmental pollution. Furthermore, such a process requires an installation of large scale and the time required for pretreatment, processing and after-treatment is very long. Accordingly, the number of man-hours required per unit is large and the manufacturing cost is correspondingly high.
- On the other hand, there have been proposed many kinds of methods for providing a metal coating on the inner sliding surface of an aluminium base cylinder by flame-spray coating and the like. In these methods, it has also been known to pre-form a molybdenum bonding layer on the base material by flame-spraying to increase the degree of bonding between the base material and the coating layer.
- In the conventional flame-spray coating, however, it has been difficult to mass-produce inexpensively cylinders having flame-sprayed coating layers of high density and high smoothness.
- According to this invention, there is provided a method of treating a sliding surface which comprises the steps of wire explosion spray coating the sliding surface of an aluminium-based alloy article using a wire made from molybdenum, a molybdenum-tungsten alloy, or tungsten to form a bonding layer; alternately and repeatedly forming on the said coating surface a layer which is formed by wire-explosion spraying using a carbon steel wire to reinforce the sliding surface and a layer which is formed by wire-explosion spraying using a wire made from molybdenum, a molybdenum-tungsten alloy, tungsten, chromium, a nickel-chromium alloy or titanium; and grinding the resultant multilayer-coated sliding surface.
- Preferably the aluminium-based alloy article is a cylinder for an internal combustion engine.
- In the accompanying drawings:—
- Figure 1 is a partially enlarged sectional view of a cylinder for use in an internal combustion engine which cylinder has been surface-treated by a method according to this invention;
- Figure 2 shows a circuit diagram of a wire-explosion spraying device used to perform wire-explosion spray coating;

Figure 3a and 3b are sectional views of a cylinder showing points at which the amount of wear is measured;

Figure 4 is a graph showing the amounts of wear in a conventional cast iron liner cylinder and a wire-explosion spray coated cylinder made according to the method of this invention.

Figure 5 is a X-ray diffraction graph of the wire-explosion spray coating layer showing the situation of nitride products of iron and titanium; and

Figures 6a and 6b are photographs, obtained by EPMA (electron probe micro-analyser), of the wire-explosion spray coating layer impregnated with  $\text{MoS}_2$ , Figure 6a showing the composition image and Figure 6b showing the characteristics X-ray image of molybdenum.

Wire-explosion spraying is a recently developed method wherein an impulsive heavy electric current is passed through a wire material to melt and atomize it in the atmosphere or an inert gas environment, the wire material being instantly melted and exploded to cause the atomized molten particles to fly at a very high speed toward a material to be coated.

This invention relates to melting and spraying specified materials onto the inner surface of a cylinder, such as an aluminium-based alloy cylinder, in a specified order by using the wire-explosion spraying mentioned above.

As mentioned above, it is known that in the case of flame-spraying coating material onto the sliding surface of an aluminium base cylinder, if a molybdenum bonding layer is pre-formed on the sliding surface by flame-spraying the molybdenum, the degree of bonding between the base material and the flame-sprayed coating material is high. However, in the case of performing wire-explosion spray coating, it is also possible to provide a bonding layer of a high bonding strength made from a high melt temperature material other than molybdenum, such as molybdenum-tungsten alloy or tungsten. Namely, molten particles of, for example molybdenum or tungsten, created by the wire-explosion spraying and having a temperature higher than the melting temperature thereof collide with the aluminium alloy base to bond with the base by a mechanical "anchor effect" and to melt a portion of the base surface layer, resulting in a mixed and diffused condition with the base material. Therefore, the bonding strength between the aluminium alloy base and the wire-explosion spray coating layer reaches above  $500 \text{ kg/cm}^2$ . This is a sufficient bonding strength against the heat cycle and mechanical shock to which the coating layer is subjected when it is used as the

sliding surface of a cylinder for an internal combustion engine. The thickness of the coating formed by one wire-explosion spraying is from 5 to  $15 \mu$ , and therefore, the number of times of the wire-explosion spraying required for obtaining a bonding layer having a required thickness is one to three times. Four or more wire explosion sprayings are unnecessary to provide such a bonding layer. A bonding layer formed from only one kind of material is not sufficient in wear resistance and seizure resistance to serve as the sliding surface of the internal combustion engine cylinder, and it is necessary to form on the bonding layer coating layers made from different materials and capable of giving required wear resistance and seizure resistance characteristics to the sliding surface.

Therefore, after forming the bonding layer by wire-explosion spraying the molybdenum wire, the molybdenum-tungsten alloy wire or the tungsten wire, a carbon steel wire is wire-explosion sprayed on the bonding layer to form a carbon steel layer which acts as a reinforcing member for the sliding surface. Next, a wire material selected from the group consisting of molybdenum wire, molybdenum-tungsten alloy wire, tungsten wire, chromium wire, nickel-chromium alloy wire and titanium wire, is wire-explosion sprayed on the carbon steel layer. Furthermore, the wire-explosion spraying of the carbon steel wire and the wire-explosion spraying of the wire material selected from the six kinds of wires are alternately and repeatedly performed to obtain a composite spray-coating layer having a thickness of from 50 to  $120 \mu$ . The two different materials mix in the composite coating layer, and the coating layer becomes a smooth coating having a uniform thickness. Finally, the surface of the composite spray-coating layer is ground and finished to form the sliding surface of the cylinder. The carbon steel contained in the complex wire-explosion spray-coating layer is martensitic and extremely hardened due to the quick cooling after wire-explosion spraying. The composite layer created from the carbon steel and the molybdenum (or molybdenum-tungsten alloy, tungsten, chromium, nickel-chromium, or titanium) has pores of a suitable porosity (3 to 5 percent). The pores act as an oil reservoir, thereby giving excellent wear resistance and seizure resistance characteristics of the sliding surface (ground surface). Figure 1 shows one example of a section of the sliding surface thus formed.

Now, embodiment of this invention will be explained. Figure 2 shows a circuit diagram of a wire-explosion spraying device used for performing wire-explosion spray

70

75

80

85

90

95

100

105

110

115

120

125

130

coating according to this invention. This device comprises a charging device CS, a charging resistor R, a capacitor C having a capacitance of, for example 90  $\mu$ F, and a discharging switch SW, as shown in the drawing. Metal material W to be sprayed is placed near the material to be coated, for example on the interior of a cylinder CYL to be coated, and is connected between output terminals of the spraying device.

First, an inner surface of an aluminium-based alloy cylinder having an inner diameter of 80.5 mm and a length of 140 mm was degrease-cleansed with perchloroethylene. A tungsten wire of 1.5 mm diameter $\times$ 180 mm length was put in the cylinder and wire-explosion sprayed to form a tungsten coating layer on the inner surface using the device mentioned above. This wire-explosion spraying was conducted at a discharge voltage of 18.9 KV. The tungsten coating layer thus formed had a thickness of about 5  $\mu$ . Next, two wire-explosion sprayed carbon steel layers were formed on the surface by separately wire-explosion spraying two piano wires (SWP—a Japanese Industrial Standard) of 1.60 mm diameter $\times$ 180 mm length in the cylinder at 14.4 KV, and thereafter one molybdenum layer was formed on the carbon steel layers by wire-explosion spraying a molybdenum wire of 1.55 mm diameter $\times$ 180 mm length in the cylinder at 17.4 KV. Thereafter, the wire-explosion spray coating of two carbon steel layers and one molybdenum layer was repeated ten times. Thereafter, the surface thus formed was ground to finish the inner surface of the aluminium-based alloy cylinder having a composite wire-explosion sprayed coating layer of a thickness of about 80  $\mu$ .

The inventors mounted the cylinder thus formed and a conventional cast iron liner cylinder and a chromium plated cylinder, respectively, on an air-cooled two stroke engine for motorcycle having the displacement of 360 cc (bore $\times$ stroke being 80.5 mm diameter $\times$ 68 mm length, and tested their performances. Figure 4 shows the amounts of wear in the cast iron liner cylinder and the wire-explosion spray coated cylinder made according to this invention. Figures 3a and 3b show the measuring points of the amount of wear, and the amounts of wear shown in Figure 4 are average values of the measured values in X and Y directions at the measuring points A, A', B and B'.

As seen from the graph shown in Figure 4, the amount of wear in the wire-explosion spray coated cylinder made according to this invention is less than a half of that in the cast iron liner cylinder, and the cylinder thus formed has sufficient endurance.

Furthermore, in the wire-explosion spray

coated cylinder made according to this invention no peeling off of the coating was found after the 200 hours endurance test. On the other hand, peeling off of the plated coating occurred in the chromium plated cylinder after about two hours running test under the same conditions.

In the wire-explosion spray coated cylinder, it is possible to reduce the thickness of the coating layer to from 100 to 50  $\mu$ , and therefore the cylinder has a high thermal conductivity and hence a high cooling performance. Furthermore, the molybdenum and the molybdenum-tungsten alloy possess self-lubrication to counter metal seizure, and the pores in the wire-explosion spray coating layer act as an oil reservoir. By the above mentioned actions and properties, the wire-explosion spray coated cylinder has a very excellent seizure resistance compared with that of the cast iron liner cylinder and chromium plated cylinder when they are used with an aluminium piston and cast iron rings.

In the case where a molybdenum-tungsten alloy wire or tungsten wire was wire-explosion sprayed onto the inner surface of an aluminium-based alloy cylinder to form a bonding layer thereon, and in the case where carbon steel wire and molybdenum-tungsten alloy wire or tungsten wire were alternately and repeatedly wire-explosion sprayed to form a composite coating layer on the bonding layer, the cylinder thus formed had substantially the same properties as that of the embodiment mentioned hereinbefore.

In the case of forming a composite coating layer using a chromium wire, a chromium wire formed by an extruding method in a powder metallurgical technique and pre-sintered and sintered in a vacuum furnace, was used as a wire to be sprayed. In this case, a multi-layer composite coating consisting of laminated chromium and carbon steel layers was formed on the bonding layer. The chromium wire-explosion spray coating layer has a Vickers hardness of from 200 to 250 and the carbon steel wire-explosion spray coating layer has a Vickers hardness of from 700 to 800. Since the different layers having this hardness exist in mixed structure in the wire-explosion spray coating composite layer, the composite layer has good wear resistance and heat resistance. Furthermore, since there is a very thin oxide film on the chromium surface, the composite layer also has an excellent seizure resistance.

In the case of using, as a nickel-chromium alloy wire, a wire made from "Chroman E" (Fe 16%, Ni, 50%, Cr 33%, Mn 1%), since the material contains a considerable amount of iron, the

formations of one carbon steel layer and one Chroman E layer were alternately and repeatedly performed by wire-explosion spraying carbon steel wires and Chroman E wires. In this case, the composite coating layer had a Vickers hardness of about 700, and had substantially the same properties as that formed when using chromium.

In the case of using a titanium wire, since the titanium coating has a small amount of titanium dioxide produced by the oxidation of titanium when the titanium wire is wire-explosion sprayed in an air atmosphere, the composite coating layer containing titanium has excellent seizure proof characteristics. Furthermore, when the cylinder having the coating layer thus formed is used in a gasoline engine, since carbon contained in the gasoline fuel reacts with titanium contained in the coating layer by the getter effect to change a portion of the titanium to TiC, the hardness of the coating is elevated and at the same time the seizure resistance characteristics of the coating are increased.

In the case of wire-explosion spraying wire materials, for example steel and titanium wires in a nitrogen gas environment, iron and titanium are partially changed to nitrides, as shown in Figure 5. Therefore, the coating layer formed by the wire-explosion spraying in the nitrogen gas environment has a Vickers hardness of from 900 to 1000. Since nitrides are excellent in connection with seizure resistance characteristics, the coating layer having these nitrides has excellent seizure resistance characteristics and also has good wear resistance characteristics.

In a modification of the present method, a composite wire material can be used which is made from different metal materials, for example, steel and molybdenum, steel and tungsten, steel and chromium, and steel and titanium. In this case, different powdered metal materials are formed by an extruding method in a powder metallurgy technique and pre-sintered and sintered in a vacuum furnace, to become a composite wire material.

Powdered raw material preferably has a suitable particle size (for example, about 5  $\mu$ ) so that the two different materials are not perfectly alloyed during sintering. Because, the characteristics of the respective materials contained in the wire material must be efficiently kept in the wire-explosion sprayed coating.

It is known that molybdenum disulfide and tungsten disulfide are extremely excellent solid lubricants. By impregnating the wire-explosion spray coating layer with these solid lubricants to fill the pores in the layer therewith, the lubrication characteristics and the seizure resistance

characteristics of the cylinder were improved.

Figures 6a and 6b are electron probe micro-analyzer photographs of a section of a coating formed by alternately and repeatedly wire-explosion spraying a piano wire and a tungsten wire onto a molybdenum bonding layer and impregnating with molybdenum disulfide, Figure 6a showing the composition image and Figure 6b showing the characteristic X-ray image of molybdenum. It will be seen from these photographs that the wire-explosion spray coating layer is impregnated with the molybdenum disulfide.

The impregnation of molybdenum disulfide particles into the wire-explosion spray coating layer was performed by impregnating the coating layer with a suspension of the molybdenum disulfide while giving an ultrasonic vibration of 10 KHz to the coating layer for a half-hour period. After the impregnating treatment, the coating layer was heat-treated at 170°C in an air atmosphere for a one hour period to strengthen the bonding of the molybdenum disulfide. A similar process is used when tungsten disulphide is used to impregnate the coating layer.

As seen from the above explanation, according to the method of this invention, a cylinder for use in an internal combustion engine having excellent wear resistance, peel resistance and seizure resistance characteristics can be obtained. Furthermore, effects attainable by this invention are as follows:

(1) Since it is unnecessary to manufacture a liner and to insert it into the cylinder, it is possible to decrease the manufacturing cost of the cylinder compared with a liner type cylinder even after the cost of wire-explosion spray coating is taken into account.

(2) The method of this invention is advantageous in connection with pretreatment, working time, after-treatment, fraction defective, and necessary installation, compared with the case of plating cylinders with chromium. In this invention, therefore, it is possible to reduce manufacturing cost by about 40% or more compared with that of chromium plated cylinders.

(3) There is no possibility of environmental pollution such as is caused by the waste liquor of a plating treatment.

(4) Since the wire-explosion spraying can be electrically controlled, it is easy to manufacture products of uniform quality and to automate the manufacturing equipment to thereby accomplish inexpensive mass production.

(5) By applying wire-explosion spray

coated cylinders to an engine, it is possible to produce an engine which is lighter than engines having the conventional cylinders.

WHAT WE CLAIM IS:—

- 5 1. A method of treating a sliding surface which comprises the steps of wire-explosion spray coating the sliding surface of an aluminium-based alloy article using a wire made from molybdenum, a molybdenum-tungsten alloy, or tungsten to form a bonding layer; alternately and repeatedly forming on the said coating surface a layer which is formed by wire-explosion spraying using a carbon steel wire to reinforce the sliding surface and a layer which is formed by wire-explosion spraying using a wire made from molybdenum, a molybdenum-tungsten alloy, tungsten, chromium, a nickel-chromium alloy or titanium; and grinding the resultant multilayer-coated sliding surface.
- 10 2. A method as claimed in claim 1, wherein a carbon steel wire and a titanium wire are alternately wire-explosion sprayed on the bonding layer in a nitrogen gas atmosphere to form and laminate alternately two kinds of nitride layers.
- 15 3. A modification of the method claimed in claim 1, wherein after the formation of the bonding layer, an alloy wire material made from steel and either molybdenum, tungsten, chromium or titanium is wire-
- 20
- 25
- 30

explosion sprayed onto the bonding layer, whereby a surface coating in which the two components exist in mixed state is obtained. 35

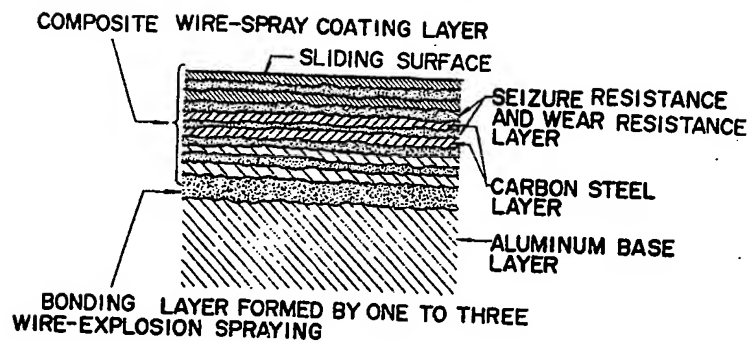
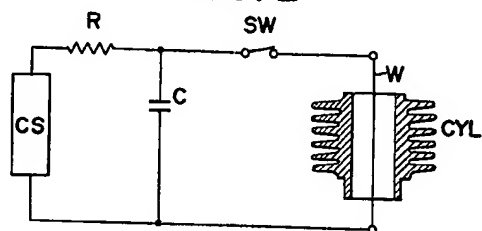
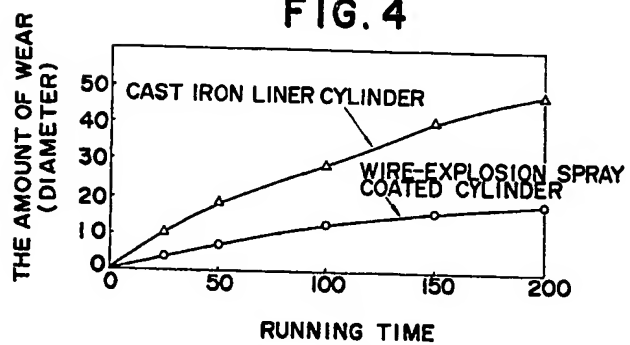
4. A method as claimed in any one of the preceding claims including the step of bringing the finished wire-explosion spray coated surface into contact with a suspension of powdered molybdenum disulfide or tungsten disulfide while subjecting the surface of the article to ultrasonic vibration so that the coating layer is impregnated with molybdenum disulfide or tungsten disulfide as a solid lubricant. 40 45

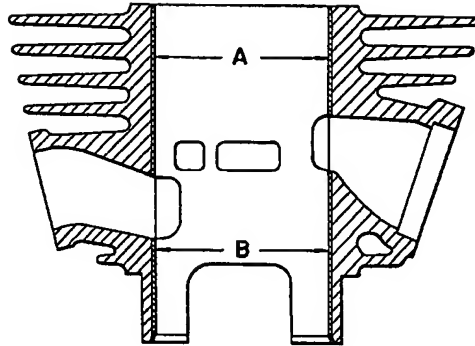
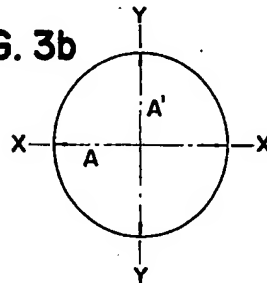
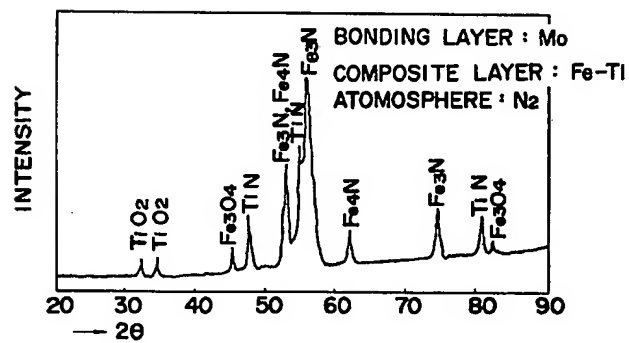
5. A method as claimed in any one of the preceding claims wherein the article to be treated is a cylinder for an internal combustion engine. 50

6. A method as claimed in claim 1 substantially as herein described with reference to the accompanying drawings.

7. An aluminium-based alloy article having a sliding surface which has been treated by a method as claimed in any one of the preceding claims. 55

KAWASAKI JUKOGYO KABU-  
SHIKI KAISHA and NIPPON  
TUNGSTEN CO., LTD.,  
Per, Boulton, Wade & Tennant,  
34, Cursitor Street,  
London EC4A 1PQ.  
Chartered Patent Agents.

**FIG. 1****FIG. 2****FIG. 4**

**FIG. 3a****FIG. 3b****FIG. 5**

**BEST AVAILABLE COPY**

1453256

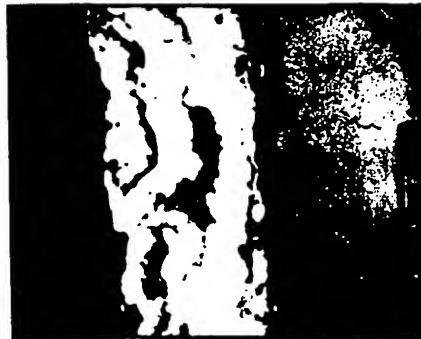
COMPLETE SPECIFICATION

3 SHEETS

*This drawing is a reproduction of  
the Original on a reduced scale*

Sheet 3

**FIG. 6a**



**FIG. 6b**

